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[Patent application]

[Title of the invention)

Intraocular lens

202220 60460001

**[Description]**

*sub 91 >* The invention relates to an intraocular lens according to the preamble of patent claim 1.

**[Prior Art]**

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An intraocular lens of this type is known from EP 0 537 643 B1. This lens may be designed as a monofocal lens, and consequently be made relatively thin, by the optical power being made up of a refractive component and a diffractive component. The cut to be made to the eye during the implantation can be kept small. Scatterings of light resulting from the diffractive fine structure component may influence the quality of the image produced on the retina.

**[Object of the invention]**

The object of the invention is to provide an intraocular lens of the type stated at the beginning in which an image with improved quality is produced on the retina with a low lens thickness.

**[Examples]**

*sub 92 >* This object is achieved according to the invention by the defining features of patent claim 1.

In the case of the intraocular lens according to the invention, arranged around a central lens area, which has

refractive properties in particular, is at least one annular lens area, which forms a common focus with the central lens area, concentric annular zones arranged around the optical lens axis being provided in the annular lens area, the difference in the path length or difference in optical path between adjacent zones being an integral multiple of the design wavelength.

In a preferred way, the design wavelength is provided in the green spectral range of visible light, in the range of 550 nm for example.

The difference in path length of the adjacent zones may be set by the refractive index or by appropriate material selection and/or the geometry of the respective zone.

In a preferred way, the curvature of the meridial section of the optical lens part is aspherically formed, the zones with the differences in path length (differences in optical path) being provided in the edge region, in which the deviation of the aspherical profile from the spherical curve has an effect.

These annular zones, which are arranged concentrically around the optical lens axis, are formed in particular in a sawtooth shape. For forming a monofocal intraocular lens, these zones have the same optical power as the central, in particular refractive, lens area. Both parts

contribute to a sharp image, which is produced on the retina of the eye.

For forming a bifocal lens, the optical lens part may be provided with an additional diffractive fine structure, which may extend over the entire optical lens part or, in a preferred way, is provided only on the central lens area, forming the refractive component. This is generally sufficient, since the bifocal function is required only when there is brightness corresponding to daylight and the pupillary aperture of the eye is essentially open only in the region of the central lens area, containing the refractive component. The additional diffractive fine structure, in particular in the form of concentric zones arranged around the optical lens axis, may be formed in such a way that adjacent zones produce a difference in path length of the optical path which is a fraction of the design wavelength, for example 0.4 or 0.6.

The invention is explained in more detail on the basis of exemplary embodiments with reference to the figures, in which:

sub A3 → figure 1 shows a sectional representation through one half of a lens body of an intraocular lens, and

figure 2 shows a graphic representation to explain an additional diffractive fine structure, for the forming of a bifocal intraocular lens.

The optical lens part 1, represented in the figures, of an intraocular lens has a central, in particular refractive, lens area 2 and a lens area 3 arranged in an annular form around the central lens area 2. The annular lens area 3 is located in an edge zone of the lens body. In the case of the exemplary embodiment represented, fine structure elements, in particular with a sawtooth shape, are arranged both on the front side and on the rear side of the lens body in concentric zones around the optical axis 6 of the lens part 1. It is also possible, however, to provide the sawtooth-like zones only on one side of the lens (front side or rear side).

Adjacent zones have a difference in path length of the respective optical path which corresponds to an integral multiple of two or more of the design wavelength. By different selection of the material in the respective adjacent annular zones and the associated different refractive indices and/or the geometry, in particular the sawtooth shape, this difference in path length of the respective optical paths can be achieved.

An outer peripheral edge 4 of the lens body has an approximately semicircular cross section, with a radius of 0.165 mm. The semicircular edge begins at a radial distance of approximately 2.835 mm from the optical axis 6. A planar straight piece 5 may be provided between the edge 4 and the

annular lens area 3 with the sawtooth-like zones. This is the case in particular whenever the outermost sawtooth zone can no longer be provided completely before the semicircular lens edge 4. The diameter of the lens is approximately 6 mm. In a preferred way, at least three annular sawtooth zones are provided in the annular lens area 3 in the vicinity of the lens edge 4.

The various curve portions are described by various functions in the respective portions.

The optical lens part is described by the following function:

$$Z_{\text{asph}}(r) = R - \sqrt{R^2 - r^2} + a_4 \cdot r^4 + a_6 \cdot r^6 + a_8 \cdot r^8 + a_{10} \cdot r^{10} + \dots \text{if } r < r_{\text{rfres\_begin}}$$

The annular lens area 3 is described by the floor function:

$$z_{\text{fres}}(r) = Z_{\text{asph}}(r) - \text{floor} \left[ \frac{Z_{\text{asph}}(r) - Z_{\text{asph}}(r_{\text{fres\_begin}})}{\text{tooth depth}} + 1 \right] \cdot \text{tooth depth}$$

if  $r_{\text{rdres\_begin}} < r < r_{\text{fres\_end}}$

The straight piece 5 is described by the straight line:

$$Z(r) = Z_{\text{asph}}(r_{\text{fres\_begin}}) \quad \text{if } r_{\text{fres\_end}} < r < r_{\text{circle\_begin}}$$

The edge region is described by a circle function with the radius  $R = 0.165$  mm:

$$Z_{\text{circle}} = Z_{\text{mpoint}} \sqrt{R^2 - (r - \chi_{\text{point}})^2} \quad \text{if } r_{\text{pmax}} < r < r_{\text{max}}$$

with  $Z_{\text{mpoint}}$  = z coordinate of the midpoint of the edge circle,

$\chi_{\text{mpoint}}$  = r coordinate of the midpoint of the edge circle.  $r_{\text{max}}$  is the maximum distance from the axis or the half diameter. With the exception of  $r_{\text{rfres\_begin}}$ , the r coordinates of the edge circle are equal in the case of all mold inserts.

In a preferred way, the zones with the differences in path length of the lens area 3 are located in the region of the deviation of the asphere from the spherical curve. The refractive component is formed by the central lens area 2, which in a preferred way has the spherical lens shape.

For forming a monofocal lens, the central lens area 2 and the annular lens area 3 are shaped in such a way that they have exactly the same focus and a common image is produced in all the zones of the optical lens part 1. The differences in the optical path length of the optical paths in adjacent zones are in this case adapted exactly to an integral multiple of an average wavelength of the visible spectrum, in particular to approximately 550 nm (design wavelength). The lens therefore produces a perfect image into the edge region. The depth of the concentric sawtooth zones is reduced here from zone to zone by 0.3  $\mu\text{m}$ .

For forming a bifocal lens, an additional diffractive fine structure is provided on the optical lens part 1. This fine structure is preferably formed as a diffractive Fresnel pattern and has the form of annular fine structure elements 7 in sawtooth shape (figure 2). Figure 2 shows the essentially spherical profile of the section curve of the central lens area, forming the refractive component 2, on one side. Starting from a refractive base curve 8, with an essentially spherical section curve profile, the diffractive annular sawtooth zones have tooth depths from 1.5  $\mu\text{m}$  to 2.8  $\mu\text{m}$ . The difference in path length between adjacent zones may be a fraction, for example 0.4 or 0.6, of the design wavelength. The additional diffractive fine structure pattern is preferably provided in the central lens area, forming the refractive component. It may, however, also extend over the annular lens area 3 and overlap the zones located in this area. As figure 2 shows, the additional diffractive fine structure elements 7, starting from the refractive base curve 8, are formed into the surface of the lens body, in particular in the central area.

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## [List of designations]

- 1 optical lens part
- 2 central lens area
- 3 annular lens area
- 4 peripheral edge
- 5 straight piece
- 6 optical axis
- 7 additional diffractive fine structure elements
- 8 refractive base curve

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